

(19) Europäisches Patentamt  
European Patent Office  
Offic ur péen d s brev ts



(11) EP 1 249 341 A1

(12)

## EUROPEAN PATENT APPLICATION

(43) Date of publication:  
16.10.2002 Bulletin 2002/42

(51) Int Cl.7: B41C 1/10, G03F 7/075

(21) Application number: 01000109.7

(22) Date of filing: 09.04.2001

(84) Designated Contracting States:  
AT BE CH CY DE DK ES FI FR GB GR IE IT LI LU  
MC NL PT SE TR  
Designated Extension States:  
AL LT LV MK RO SI

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### (54) Lithographic printing plate precursor

(57) A positive-working lithographic printing plate precursor comprising a support having a hydrophilic surface and a coating comprising a first layer closest to the support, said first layer containing an oleophilic phenolic resin soluble in an aqueous alkaline developer, and a second layer containing a polysiloxane compound, wherein

(a) the second layer is capable of preventing the aqueous alkaline developer from penetrating into the first layer to an extent that substantially no dis-

solution of unexposed coating occurs upon immersion in the aqueous alkaline developer during a time period  $t_2$ :

(b) and wherein said capability of the second layer of preventing the aqueous alkaline developer from penetrating into the first layer is reduced upon exposure to heat or light to an extent that substantially complete dissolution of exposed coating occurs upon immersion in the aqueous alkaline developer during a time period  $t_1$ ;

and wherein  $t_2 > t_1$  and  $t_2 - t_1$  is at least 10 seconds.

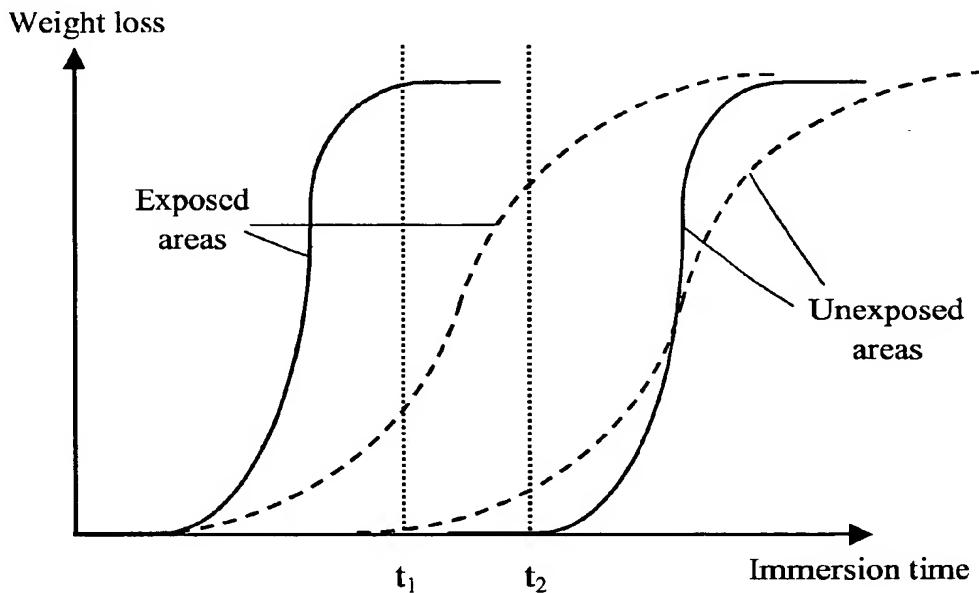


Fig. 1

**D**escription

## FIELD OF THE INVENTION

5 [0001] The present invention relates to a positive working lithographic printing plate precursor suitable for computer-to-plate methods.

## BACKGROUND OF THE INVENTION

10 [0002] Lithographic printing presses use a so-called printing master such as a printing plate which is mounted on a cylinder of the printing press. The master carries a lithographic image on its surface and a print is obtained by applying ink to said image and then transferring the ink from the master onto a receiver material, which is typically paper. In conventional lithographic printing, ink as well as an aqueous fountain solution (also called dampening liquid) are supplied to the lithographic image which consists of oleophilic (or hydrophobic, i.e. ink-accepting, water-repelling) areas as well as hydrophilic (or oleophobic, i.e. water-accepting, ink-repelling) areas. In so-called driographic printing, the 15 lithographic image consists of ink-accepting and ink-abhesive (ink-repelling) areas and during driographic printing, only ink is supplied to the master.

20 [0003] Printing masters are generally obtained by the so-called computer-to-film method wherein various pre-press steps such as typeface selection, scanning, color separation, screening, trapping, layout and imposition are accomplished digitally and each color selection is transferred to graphic arts film using an image-setter. After processing, the film can be used as a mask for the exposure of an imaging material called plate precursor and after plate processing, a printing plate is obtained which can be used as a master.

25 [0004] A typical printing plate precursor for computer-to-film methods comprise a hydrophilic support and an image-recording layer of a photosensitive polymer layers which include UV-sensitive diazo compounds, dichromate-sensitized hydrophilic colloids and a large variety of synthetic photopolymers. Particularly diazo-sensitized systems are widely used. Upon image-wise exposure, typically by means of a film mask in a UV contact frame, the exposed image areas become insoluble and the unexposed areas remain soluble in an aqueous alkaline developer. The plate is then processed with the developer to remove the diazonium salt or diazo resin in the unexposed areas. So the exposed areas define the image areas (printing areas) of the printing master, and such printing plate precursors are therefore called 30 'negative-working'. Also positive-working materials, wherein the exposed areas define the non-printing areas, are known, e.g. plates having a novolac/naphtoquinone-diazide coating which dissolves in the developer only at exposed areas.

35 [0005] In addition to the above photosensitive materials, also heat-sensitive printing plate precursors are known. Such materials offer the advantage of daylight stability and are especially used in the so-called computer-to-plate method wherein the plate precursor is directly exposed, i.e. without the use of a film mask. The material is exposed to heat or to infrared light and the generated heat triggers a (physico-)chemical process, such as ablation, polymerization, insolubilization by cross-linking of a polymer, decomposition, or particle coagulation of a thermoplastic polymer latex.

40 [0006] US 5,466,557 describes a positive-working printing plate precursor which is sensitive to both ultraviolet (UV) and infrared (IR) light but not to visible light, comprising a support and a coating comprising an oleophilic polymer that is soluble in an aqueous alkaline developer and a latent Bronsted acid.

[0007] EP-A 864420 describes a positive-working heat-sensitive printing plate precursor comprising a support, a first layer containing an oleophilic polymer that is soluble in an aqueous alkaline developer and an IR-sensitive top layer of which the penetrability by or solubility in the aqueous alkaline developer is changed upon exposure to IR light.

45 [0008] WO 97/39894 describes a positive-working heat-sensitive printing plate precursor which is sensitive to IR light but not to UV light comprising a support and an IR-sensitive coating comprising an oleophilic polymer that is soluble in an aqueous alkaline developer and a dissolution inhibitor which reduces the solubility of the polymer in the developer.

50 [0009] The major problem associated with the prior art materials is the low differentiation between the development kinetics of exposed and non-exposed areas, i.e. the dissolution of the exposed coating in the developer is not completely finished before the unexposed coating also starts dissolving in the developer. This leads to low quality prints showing unsharp edges and toning (ink-acceptance in exposed areas).

## SUMMARY OF THE INVENTION

55 [0010] It is an aspect of the present invention to provide a positive-working lithographic printing plate precursor which shows a high differentiation between exposed and non-exposed areas. A printing plate precursor as defined in claim 1 exhibits a rapid dissolution of exposed areas in the aqueous alkaline developer and a much slower dissolution of the non-exposed areas. At the first time period designated as  $t_1$  in Fig. 1, the exposed areas are completely dissolved,

whereas dissolution of the non-exposed areas starts later, after the second time period designated as  $t_2$  in Fig. 1. The development latitude, defined as the time difference  $t_2 - t_1$ , is at least 10 seconds, more preferably at least 20 seconds and most preferably at least 40 seconds.

[0011] Further advantages and embodiments of the present invention will become apparent from the following description.

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#### BRIEF DESCRIPTION OF THE DRAWING

[0012] Fig. 1 shows schematically the development kinetics, expressed as weight loss of the coating during development, of exposed and non-exposed areas of a positive-working lithographic printing plate precursor according to the invention (solid lines) and of a material which does not comply with the requirements of the invention (dashed lines).

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#### DETAILED DESCRIPTION OF THE INVENTION

[0013] The lithographic printing plate precursor of the present invention contains a support having a hydrophilic surface and a coating provided thereon. The coating comprises at least two layers, designated herein as first and second layer, the first layer being closest to the support, i.e. located between the support and the second layer. The printing plate precursor is positive-working, i.e. after exposure and development the exposed areas of the coating are removed from the support and define hydrophilic (non-printing) areas, whereas the unexposed coating is not removed from the support and defines an oleophilic (printing) area. The second layer acts as a barrier which prevents penetration of the aqueous alkaline developer into the phenolic resin of the first layer at unexposed areas. At exposed areas, the barrier function of the second layer is reduced due to the exposure and dissolution of the coating at those areas occurs rapidly upon immersion in an aqueous alkaline developer. This 'switching off' of the barrier function of the second layer upon exposure can be tested e.g. by measuring the water uptake, due to swelling of the phenolic resin, of an exposed and a non-exposed sample : typically, the exposed sample absorbs a substantial amount of water whereas the average water-uptake of non-exposed samples is within statistical error not different from zero.

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[0014] The barrier function of the second layer arises from the presence of a polysiloxane. The siloxane may be present in an amount of e.g. between 0.5 and 15 mg/m<sup>2</sup>, preferably between 0.5 and 10 mg/m<sup>2</sup>, more preferably between 0.5 and 5 mg/m<sup>2</sup> and most preferably between 0.5 and 2 mg/m<sup>2</sup>. Since the polysiloxane is ink-repelling, higher amounts than 15 mg/m<sup>2</sup> can result in poor ink-acceptance of the non-exposed areas. An amount lower than 0.5 mg/m<sup>2</sup> on the other hand may lead to an unsatisfactory development latitude, as shown by the dashed curves in Fig. 1 : development of the exposed areas is not completed before the start of the development of the non-exposed areas.

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The S-shaped curves in Fig. 1 reach a plateau when the coating is completely dissolved and, as a result, no further weight loss is measured. A material according to the invention (solid lines in Fig. 1) shows a substantially complete dissolution of the exposed areas after a development time  $t_1$ , whereas substantially no dissolution of the non-exposed areas occurs until  $t_2$ . "Substantially complete dissolution" shall be understood as a degree of dissolution of the coating which is sufficient to preclude toning, due to ink-acceptance of exposed coating that remains on the support after development. "Substantially no dissolution" shall be understood as a degree of dissolution which does not lead to a prohibitive reduction of the ink coverage on the prints, which is especially noticeable at the edges of the printing areas.

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Sharp edges and no toning are preferred characteristics of prints produced by the materials of the present invention.

[0015] The second layer may contain the phenolic resin as well as the polysiloxane. However, in a preferred embodiment, the second layer consists essentially of polysiloxane. The polysiloxane may be a linear, cyclic or complex cross-linked polymer or copolymer. Preferred siloxanes are phenylalkylsiloxanes and dialkylsiloxanes. The number of siloxane groups  $-Si(R,R')-O-$  in the (co-)polymer is at least 2, preferably at least 10, more preferably at least 20. It may be less than 100, preferably less than 60. The polysiloxane compound is preferably a random or block-copolymer comprising siloxane and alkyleneoxide groups, suitably comprising about 15 to 25 siloxane units and 50 to 70 alkyleneoxide groups. Preferred polysiloxanes include a copolymer of dimethyldichlorosilane, ethylene oxide and propylene oxide.

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[0016] In a preferred embodiment, the barrier function of the second layer can also be reduced by simple rubbing. A preferred polysiloxane containing second layer is capable of being removed by rubbing to an extent that substantially complete dissolution of rubbed coating occurs upon immersion in the aqueous alkaline developer during a time period  $t_3$  of 10 seconds, said rubbing being defined as rubbing with a cotton pad of a size 85 x 85 mm at a pressure of 9.69 g/cm<sup>2</sup> during 50 cycles, each cycle being defined as a linear translation of the cotton pad on the coating over a distance of 30 cm at a speed of 0.40 m/s. Said distance is the distance between the position of the tailing edge at the beginning of a translation and the position of the leading edge at the end of a translation. The cotton pad is preferably of the type 4-4931 from A.B. Dick.

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[0017] Whilst the applicants do not wish to be limited by any theoretical explanation of how their invention operates, it is believed that the spreading of the second layer on the first layer is reduced by the exposure, e.g. by 'thermal de-

wetting', i.e. heat-induced decrease of the surface tension of the polysiloxane, to such an extent that the second layer breaks up, thereby forming an incomplete layer which can no longer shield the first layer from the developer completely. Rubbing with a cotton pad also removes a sufficient amount of the polysiloxane to trigger development. The removal of the polysiloxane by rubbing can be measured e.g. by comparing the ratio of the siloxane  $^1\text{H-NMR}$  signals versus the signals of the phenolic resin of a sample before and after rubbing.

[0018] The phenolic resin is an oleophilic polymer that is soluble in an aqueous developer, more preferably an aqueous alkaline developing solution with a pH between 7.5 and 14. Preferred polymers are e.g. novolac, resoles, polyvinyl phenols and carboxy substituted. Typical examples of these polymers are described in DE-A-4007428, DE-A-4027301 and DE-A-4445820.

[0019] The coating preferably comprises a dye or pigment which sensitizes the material to the light used during the exposure. It is preferably a compound or particle having an absorption maximum in the wavelength range between 250 and 1500 nm. According to a more preferred embodiment, the material is sensitive to UV light (<400 nm, most preferably between 300 and 400 nm) and/or IR light (>750 nm) but not to visible light (400-750 nm), so that a daylight stable material is obtained which can be handled without the need for darkroom conditions. "Not sensitive to visible light" means that no substantial dissolution in the developer is induced by exposure to visible light. Preferred IR-absorbing compounds are dyes such as cyanine dyes or pigments such as carbon black. Preferred UV-absorbing compounds are capable of generating a radical upon exposure to UV light. Suitable UV-sensitizers can be selected from the group consisting of a compound having a carbon-halogen bond, an aromatic onium salt, an organic peroxide, a thio compound, a hexaarylbisimidazole or a ketoxime ester. Specific examples of such compounds can be found in US 5,049,481 and 5,466,557. Preferably s-triazines, thioxanthones, hexaaryl-bisimidazoles or mercaptobenzoxazoles are used.

[0020] The sensitizing dye or pigment may be present in the first and/or the second layer. According to a highly preferred embodiment, the dye or pigment is concentrated in or near the second layer, e.g. in an intermediate layer between the first and the second layer. According to that embodiment, said intermediate layer comprises the light absorbing compound in an amount higher than the amount of light absorbing compound in the first or in the second layer. In a preferred embodiment, the second layer consists essentially of polysiloxane, i.e. comprises no effective amount of sensitizing dye.

[0021] The first layer may further contain other ingredients such as additional binders, colorants, development inhibitors as disclosed in WO 97/39894 or accelerators such as 3,4,5-trimethoxybenzoic acid. Said colorants are preferably dyes which during development remain in the coating at non-exposed areas and which are washed out at exposed areas, thereby producing a visible image. Such indicator dyes preferably do not sensitize the coating to visible light.

[0022] The support has a hydrophilic surface or is provided with a hydrophilic layer. The support may be a sheet-like material such as a plate or it may be a cylindrical element such as a sleeve which can be slid around a print cylinder of a printing press. Preferably, the support is a metal support such as aluminum or stainless steel.

[0023] A particularly preferred lithographic support is an electrochemically grained and anodized aluminum support. The anodized aluminum support may be treated to improve the hydrophilic properties of its surface. For example, the aluminum support may be silicated by treating its surface with a sodium silicate solution at elevated temperature, e.g. 95°C. Alternatively, a phosphate treatment may be applied which involves treating the aluminum oxide surface with a phosphate solution that may further contain an inorganic fluoride. Further, the aluminum oxide surface may be rinsed with a citric acid or citrate solution. This treatment may be carried out at room temperature or may be carried out at a slightly elevated temperature of about 30 to 50°C. A further interesting treatment involves rinsing the aluminum oxide surface with a bicarbonate solution. Still further, the aluminum oxide surface may be treated with polyvinylphosphonic acid, polyvinylbenzenesulfonic acid, sulfuric acid esters of polyvinyl alcohol, polyvinylsulfonic acid, polyvinylbenzenesulfonic acid, polyvinylmethylphosphonic acid, phosphoric acid esters of polyvinyl alcohol, polyvinylsulfonic acid, polyvinylbenzenesulfonic acid, sulfuric acid esters of polyvinyl alcohol, and acetals of polyvinyl alcohols formed by reaction with a sulfonated aliphatic aldehyde. It is further evident that one or more of these post treatments may be carried out alone or in combination. More detailed descriptions of these treatments are given in GB-A- 1 084 070, DE-A- 4 423 140, DE-A- 4 417 907, EP-A- 659 909, EP-A- 537 633, DE-A- 4 001 466, EP-A- 292 801, EP-A- 291 760 and US-P- 4 458 005.

[0024] According to another embodiment, the support can also be a flexible support, which is provided with a hydrophilic layer, hereinafter called 'base layer'. The flexible support is e.g. paper, plastic film, thin aluminum or a laminate thereof. Preferred examples of plastic film are polyethylene terephthalate film, polyethylene naphthalate film, cellulose acetate film, polystyrene film, polycarbonate film, etc. The plastic film support may be opaque or transparent.

[0025] The base layer is preferably a cross-linked hydrophilic layer obtained from a hydrophilic binder cross-linked with a hardening agent such as formaldehyde, glyoxal, polyisocyanate or a hydrolyzed tetra-alkylorthosilicate. The latter is particularly preferred. The thickness of the hydrophilic base layer may vary in the range of 0.2 to 25  $\mu\text{m}$  and is preferably 1 to 10  $\mu\text{m}$ .

[0026] The hydrophilic binder for use in the base layer is e.g. a hydrophilic (co)polymer such as homopolymers and

copolymers of vinyl alcohol, acrylamide, methylol acrylamide, methylol methacrylamide, acrylate acid, methacrylate acid, hydroxyethyl acrylate, hydroxyethyl methacrylate or maleic anhydride/vinylmethylether copolymers. The hydrophilicity of the (co)polymer or (co)polymer mixture used is preferably the same as or higher than the hydrophilicity of polyvinyl acetate hydrolyzed to at least an extent of 60% by weight, preferably 80% by weight.

[0027] The amount of hardening agent, in particular tetraalkyl orthosilicate, is preferably at least 0.2 parts per part by weight of hydrophilic binder, more preferably between 0.5 and 5 parts by weight, most preferably between 1 parts and 3 parts by weight.

[0028] The hydrophilic base layer may also contain substances that increase the mechanical strength and the porosity of the layer. For this purpose colloidal silica may be used. The colloidal silica employed may be in the form of any commercially available water dispersion of colloidal silica for example having an average particle size up to 40 nm, e.g. 20 nm. In addition inert particles of larger size than the colloidal silica may be added e.g. silica prepared according to Stöber as described in J. Colloid and Interface Sci., Vol. 26, 1968, pages 62 to 69 or alumina particles or particles having an average diameter of at least 100 nm which are particles of titanium dioxide or other heavy metal oxides. By incorporating these particles the surface of the hydrophilic base layer is given a uniform rough texture consisting of microscopic hills and valleys, which serve as storage places for water in background areas.

[0029] Particular examples of suitable hydrophilic base layers for use in accordance with the present invention are disclosed in EP-A- 601 240, GB-P- 1 419 512, FR-P- 2 300 354, US-P- 3 971 660, and US-P- 4 284 705.

[0030] It is particularly preferred to use a film support to which an adhesion improving layer, also called support layer, has been provided. Particularly suitable adhesion improving layers for use in accordance with the present invention comprise a hydrophilic binder and colloidal silica as disclosed in EP-A- 619 524, EP-A- 620 502 and EP-A- 619 525. Preferably, the amount of silica in the adhesion improving layer is between 200 mg/m<sup>2</sup> and 750 mg/m<sup>2</sup>. Further, the ratio of silica to hydrophilic binder is preferably more than 1 and the surface area of the colloidal silica is preferably at least 300 m<sup>2</sup>/gram, more preferably at least 500 m<sup>2</sup>/gram.

[0031] The printing plate precursor of the present invention can be exposed to heat or to light, e.g. by means of a thermal head, LEDs or a laser head. Preferably, one or more lasers such as a He/Ne laser, an Ar lasers or a violet laser diode are used. Most preferably, the light used for the exposure is not visible light, e.g. UV (laser) light or a laser emitting near infrared light having a wavelength in the range from about 750 to about 1500 nm is used, such as a semiconductor laser diode, a Nd:YAG or a Nd:YLF laser. The required laser power depends on the sensitivity of the image-recording layer, the pixel dwell time of the laser beam, which is determined by the spot diameter (typical value of modern plate-setters at 1/e<sup>2</sup> of maximum intensity : 10-25 µm), the scan speed and the resolution of the exposure apparatus (i.e. the number of addressable pixels per unit of linear distance, often expressed in dots per inch or dpi; typical value : 1000-4000 dpi).

[0032] Two types of laser-exposure apparatuses are commonly used: internal (ITD) and external drum (XTD) plate-setters. ITD plate-setters for thermal plates are typically characterized by a very high scan speed up to 500 m/sec and may require a laser power of several Watts. XTD plate-setters for thermal plates having a typical laser power from about 200 mW to about 1 W operate at a lower scan speed, e.g. from 0.1 to 10 m/sec.

[0033] The known plate-setters can be used as an off-press exposure apparatus, which offers the benefit of reduced press down-time. XTD plate-setter configurations can also be used for the on-press exposure, offering the benefit of immediate registration in a multicolor press. More technical details of on-press exposure apparatuses are described in e.g. US 5,174,205 and US 5,163,368.

[0034] In the development step, the non-exposed areas of the coating are removed by immersion in an aqueous alkaline developer, which may be combined with mechanical rubbing, e.g. by a rotating brush. The development step may be followed by a drying step, a rinsing step, a gumming step, and/or a post-baking step.

[0035] The printing plate thus obtained can be used for conventional, so-called wet offset printing, in which ink and an aqueous dampening liquid is supplied to the plate. Another suitable printing method uses so-called single-fluid ink without a dampening liquid. Single-fluid inks which are suitable for use in the method of the present invention have been described in US 4,045,232 and US 4,981,517. In a most preferred embodiment, the single-fluid ink comprises an ink phase, also called the hydrophobic or oleophilic phase, and a polyol phase as described in WO 00/32705.

## EXAMPLES

### Preparation of the lithographic base

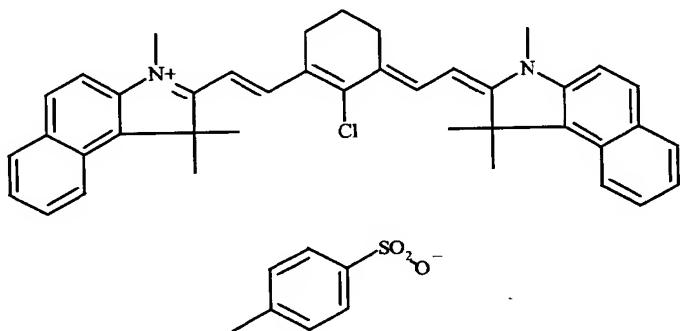
[0036] A 0.30 mm thick aluminum foil was degreased by immersing the foil in an aqueous solution containing 5 g/l of sodium hydroxide at 50°C and rinsed with demineralized water. The foil was then electrochemically grained using an alternating current in an aqueous solution containing 4 g/l of hydrochloric acid, 4 g/l of hydroboric acid and 5 g/l of aluminum ions at a temperature of 35°C and a current density of 1200 A/m<sup>2</sup> to form a surface topography with an average center-line roughness Ra of 0.5 µm.

[0037] After rinsing with demineralized water the aluminum foil was then etched with an aqueous solution containing 300 g/l of sulfuric acid at 60°C for 180 seconds and rinsed with demineralized water at 25°C for 30 seconds.

[0038] The foil was subsequently subjected to anodic oxidation in an aqueous solution containing 200 g/l of sulfuric acid at a temperature of 45°C, a voltage of about 10 V and a current density of 150 A/m<sup>2</sup> for about 300 seconds to form an anodic oxidation film of 3.00 g/m<sup>2</sup> of Al<sub>2</sub>O<sub>3</sub> then washed with demineralized water, post-treated with a solution containing polyvinylphosphonic acid and subsequently with a solution containing aluminum trichloride, rinsed with demineralized water at 20°C during 120 seconds and dried.

#### Preparation of a lithographic printing plate precursor

[0039] An IR-sensitive layer was coated onto the above described lithographic base from a tetrahydrofuran/methoxypropanol mixture (50:50 vol. ratio) at 20 µm coating thickness. After drying the layer consisted of 0.13 g/m<sup>2</sup> of 3,4,5-trimethoxybenzoic acid, 35 mg/m<sup>2</sup> of infrared dye IR-1, 0.9 g/m<sup>2</sup> of ALNOVOL SPN452 (novolac available from Clariant, Germany) and 13 mg/m<sup>2</sup> of Flexobleu 630 (an indicator dye available from BASF).



IR-1

[0040] Then, a second coating of 5 mg/m<sup>2</sup> of a polysiloxane polyether copolymer (TEGO GLIDE 410, commercially available from Tego Chemie Service GmbH) was applied on the first layer using isopropanol/water (25:75 vol. ratio) as a solvent.

[0041] This material was imaged with a TRENDSETTER 3244-T (available from Creo) external drum platesetter operation at 830 nm, 2400 dpi, 150 rpm resulting in an energy-density of 140 mJ/cm<sup>2</sup>. After IR-imaging the material was developed during 25 seconds in an Autolith T processor (available from Agfa-Gevaert) using an OZASOL EP26 developer (also available from Agfa-Gevaert) at 25°C. The processor also contained a rinsing section (water) and a gumming section (RC795 gum from Agfa-Gevaert). The IR-exposed areas dissolved very rapidly without any attack in the non IR-exposed areas, resulting in a positive working printing plate. The plate was printed on a Heidelberg GTO46 printing machine with a conventional ink (K+E800) and fountain solution (Rotamatic), resulting in good prints, i.e. no toning in the exposed areas and good ink-uptake in the non imaged areas.

Comparative example.

[0042] In this comparative example an imaging element was prepared in an identical way as the imaging element of example 1 with the exception that no second coating was applied on the first layer.

[0043] This material was imaged with a CREO TRENDSETTER 3244-T™ external drum platesetter at 2400 dpi with an energy-density of 263 mJ/cm<sup>2</sup> at 106 rpm. After IR-imaging the material was developed as described in the previous example. The IR-exposed areas and the non-exposed areas were both dissolved in the developer, resulting in a useless printing plate without image. Development in milder conditions (8 parts EP26 / 2 parts water) did not provide an improvement.

**Claims**

1. A positive-working lithographic printing plate precursor comprising a support having a hydrophilic surface and a coating comprising a first layer closest to the support, said first layer containing an oleophilic phenolic resin soluble in an aqueous alkaline developer, and a second layer containing a polysiloxane compound, wherein
  - (c) the second layer is capable of preventing the aqueous alkaline developer from penetrating into the first layer to an extent that substantially no dissolution of unexposed coating occurs upon immersion in the aqueous alkaline developer during a time period  $t_2$ ;
  - (d) and wherein said capability of the second layer of preventing the aqueous alkaline developer from penetrating into the first layer is reduced upon exposure to heat or light to an extent that substantially complete dissolution of exposed coating occurs upon immersion in the aqueous alkaline developer during a time period  $t_1$ ;  
and wherein  $t_2 > t_1$  and  $t_2 - t_1$  is at least 10 seconds.
2. A lithographic printing plate precursor according to claim 1 wherein the amount of the polysiloxane compound is between 0.5 and 15 mg/m<sup>2</sup>.
3. A lithographic printing plate precursor according to claim 1 wherein the amount of the polysiloxane compound is between 0.5 and 10 mg/m<sup>2</sup>.
4. A lithographic printing plate precursor according to claim 1 wherein the amount of the polysiloxane compound is between 0.5 and 5 mg/m<sup>2</sup>.
5. A lithographic printing plate precursor according to claim 1 wherein the amount of the polysiloxane compound is between 0.5 and 2 mg/m<sup>2</sup>.
6. A lithographic printing plate precursor according to any of the preceding claims wherein the second layer consists essentially of the polysiloxane compound.
7. A lithographic printing plate precursor according to any of the preceding claims wherein  $t_1$  is 20 and  $t_2$  is 40 seconds.
8. A lithographic printing plate precursor according to any of the preceding claims wherein  $t_1$  is 10 and  $t_2$  is 60 seconds.
9. A lithographic printing plate precursor according to any of the preceding claims wherein the second layer is capable of being removed by rubbing to an extent that substantially complete dissolution of rubbed coating occurs upon immersion in the aqueous alkaline developer during a time period  $t_3$  of 10 seconds, said rubbing being defined as rubbing with a cotton pad of a size 85 x 85 mm at a pressure of 9.69 g/cm<sup>2</sup> during 50 cycles, each cycle being defined as a linear translation of the cotton pad on the coating over a distance of 30 cm at a speed of 0.40 m/s.
10. A lithographic printing plate precursor according to claim 9 wherein  $t_3$  is 20 seconds.
11. A lithographic printing plate precursor according to any of the preceding claims wherein the light is infrared light and wherein the coating is not sensitive to visible light.
12. A lithographic printing plate precursor according to any of claims 1 to 10 wherein the light is ultraviolet light and wherein the coating is not sensitive to visible light.
13. A lithographic printing plate precursor according to claim 12 wherein the ultraviolet light is light having a wavelength between 250 and 400 nm.
14. A lithographic printing plate precursor according to any of the preceding claims further comprising an intermediate layer between said first and second layer, said intermediate layer comprising a dye or pigment in an amount higher than the amount of dye or pigment in the first and in the second layer.
15. A lithographic printing plate precursor according to any of the preceding claims wherein the second layer is substantially free of dye or pigment.

**EP 1 249 341 A1**

16. A method of making a lithographic printing plate comprising the steps of image-wise exposure of a lithographic printing plate precursor according to any of the preceding claims and subsequent processing with the aqueous alkaline developer during a development time between  $t_1$  and  $t_2$ .
- 5      17. A method of lithographic printing with a printing plate obtained by the method of claim 16.

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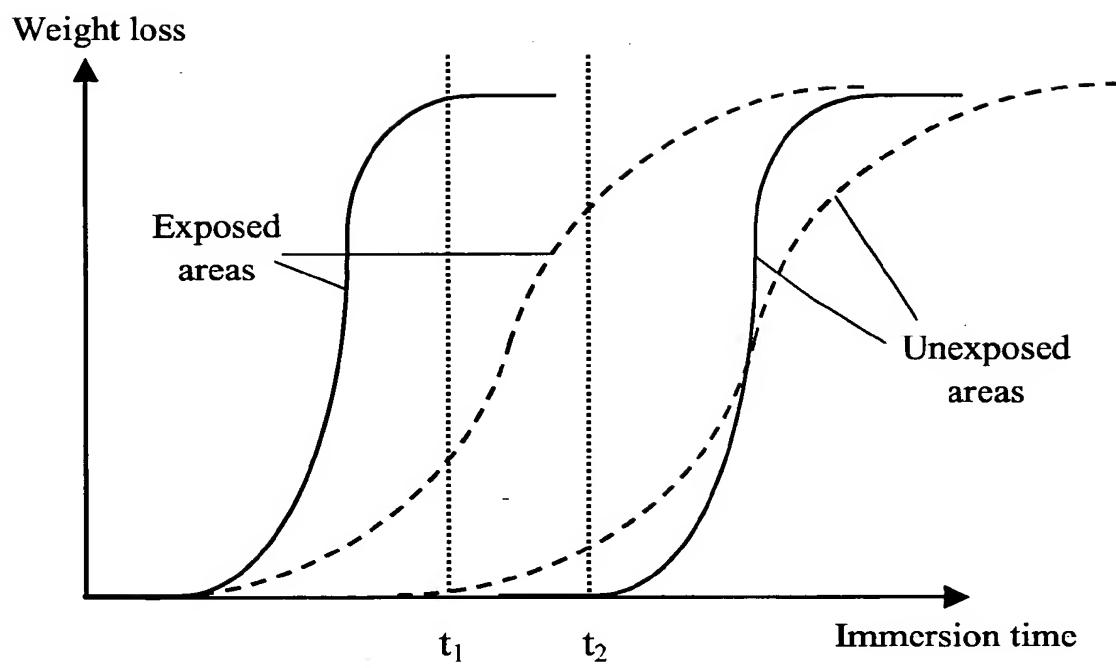


Fig. 1



European Patent  
Office

## EUROPEAN SEARCH REPORT

Application Number  
EP 01 00 0109

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
X	EP 0 950 514 A (AGFA-GEVAERT NAAMLOZE VENNOOTSCHAP ) 20 October 1999 (1999-10-20) * claims 1,6,7; examples 1-5 * * page 4, line 43 - line 45 * * page 4, line 52 - line 56 *	1-17	B41C1/10 G03F7/075
X	EP 0 940 266 A (AGFA-GEVAERT NAAMLOZE VENNOOTSCHAP ) 3 September 1999 (1999-09-08) * claims 1,9,10; examples 1-9 * * page 6, line 33 - line 34 * * page 6, line 42 - line 47 *	1-17	
X	PATENT ABSTRACTS OF JAPAN vol. 008, no. 265 (P-318), 5 December 1984 (1984-12-05) & JP 59 135471 A (TORAY KK), 3 August 1984 (1984-08-03) * abstract *	1-17	
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